

## *ECET 4530*

*Industrial Motor Control*

*Starting Induction Motors*

### **Across-the-Line Motor Starting**

**Across-the-Line starting** of an induction motor involves starting the motor with full-rated voltage applied across its terminals.



**When the main contacts close, the motor's terminals are connected directly to the source terminals, and thus:**

$$
\widetilde{V}_{motor} = \widetilde{V}_{source}
$$







### **Predicting the Locked-Rotor Current**

As per **Table 31** of the NEMA **MG-1 Standard**, the nominal **locked-rotor current** for a 3Φ, **230V**, **150hp**, induction motor is **2170A**.

But our motor is rated at **460V**.

The footnote at the bottom of the table specifies how to account for the different voltages.



Table 31<br>LOCKED-ROTOR CURRENT OF 3-PHASE 60-HERTZ SMALL AND





### **Adverse Effects of Starting Current**

The **adverse effects** associated with the large currents that are drawn into a motor during startup include:

- A **torque surge** developed by the motor that can be damaging to the motor's connected mechanical load.
- A **voltage drop in the supply network** that may affect the operation of other devices.

Whether these currents are short-lived during a successful startup or extended in length during a problematic/failed startup, their effects should be considered in order to determine if they need to be mitigated by the motor control system.

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### **Induction Motor Starting Methods**

A variety of different methods have been developed to mitigate the undesirable effects that are associated with the large currents that are normally drawn when starting an induction motor.

They include:

- **Reduced Voltage Starting**
- **Partial Winding Starting**
- **Reduced Frequency Starting**

*Note – reduced frequency starting using Variable Frequency Drives (VFDs) is covered in a later presentation.*







### **Series-Resistance Motor Starters**

Once the motor has had a chance to accelerate to the point at which the currents drawn by the motor would have decreases to an acceptable level if supplied at rated voltage, the **resistors** must then be **electrically removed from the circuit** so as not to impair the motor's operation under normal use.

A **contactor** is typically employed to provide this service.



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### **L1 L3 L2 N 3 Power Source Start Resistor Resistor Resistor Stop S = "Start" Contactor R = "Run" Contactor Run S S S S S S T1 3 Induction Motor R R R R R Series Resistance Starter with Manual (2-Step) Control Circuit** When "**Run**" is **pressed**, the "**R**" **coil** is **energized**, in-turn **actuating the "R" contacts** to **bypass the resistors** and **supply the motor at full-voltage**. **Series-Resistance Starter Operation**





### **Series-Resistance Starter Operation**

**Series Resistance Starter** with **Manual (2-Step) Control Circuit** What if "**Start**" **and** "**Run**" **are pressed at the same time?**



























### **Determining the Series-Resistor Value**

### **Series Resistance Determination**

- By setting the **locked-rotor test voltage** to **½ rated voltage**, the locked-rotor test will draw half of the current that would be drawn if full-voltage was applied.
- The **50% reduction** in locked-rotor current will **decrease** both the **heat generated** and the **torque developed** during the test **by 75%**.







### **Series-Resistor Value Example**

**Series Resistance Calculation Example**

A **locked-rotor test** is performed on the motor with **½-rated voltage applied per phase** during the test.

The **per-phase test results** are as follows:

 $V_{LR} = 60V, I_{LR} = 2.1A, P_{10} = 90W$ 

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**Series Resistance Calculation Example Desired starting current:**  $I_{\text{line}} = 2.4 A$  $(R_{\rm ext}+R_{\rm LR})^2+(X_{\rm LR})^2$  $(R_{\scriptscriptstyle\rm{ext}}+20.4)^2+(20)$ *A R ext A*  $(R_{ext} + R_{LR})^2 + (X$ *V Z V*  $\left| \tilde{I}_{line} \right| = I$  $ext{ } \perp \mathbf{\Lambda}_{LR}$   $\perp$   $\perp \mathbf{\Lambda}_{LR}$ *ph eq ph*  $\widetilde{I}_{line} = I_{line} = \frac{\left| \widetilde{V}_{ph} \right|}{\left| \sigma \right|} = \frac{V_{ph}}{\sqrt{2\pi R_0^2 + \left( \frac{\sigma^2}{2} \right)^2 + \left( \frac{\sigma^2}{2} \right)^2}} = 2.4$ 2.4  $(20.4)^2 + (20)$ 120  $\frac{1}{(20)^2}$  $\frac{1}{2+(y-1)^2}$  $+20.4)^{2}$  +  $\Rightarrow$  $+ R_{IR}^2)^2 +$  $= I_{line} = \frac{|P^n|}{|P^n|} =$ **Series-Resistor Value Example**  $\tilde{\mathbf{r}}_{\text{line}}$  **R**<sub>Ext</sub> **R**<sub>LR</sub> **jX**<sub>LR</sub>  $\tilde{v}_{ph}$  $R_{ext}$   $R_{LR}$   $jX_{LR}$ 42













