



ECET 2111

Circuits II

Three Phase Systems

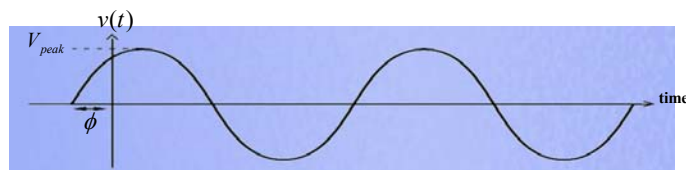
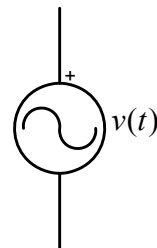


Single-Phase AC Voltage Sources

A (single-phase) **AC voltage source** is a source whose voltage varies sinusoidally, as defined by the function:

$$v(t) = V_{peak} \cdot \sin(\omega \cdot t + \phi)$$

where: V_{peak} is the peak value of the voltage,
 ω is the angular frequency ($2\pi f$) of the waveform, and
 ϕ is the phase angle of the waveform.



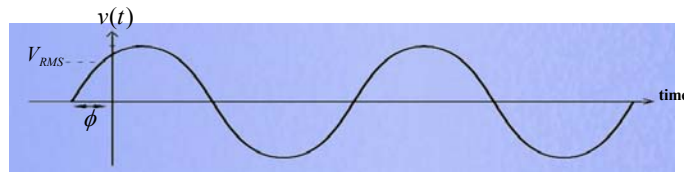
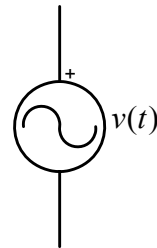


Single-Phase AC Voltage Sources

The voltage waveform may also be expressed in terms of its **RMS voltage magnitude**:

$$v(t) = \sqrt{2} \cdot V_{RMS} \cdot \sin(\omega \cdot t + \phi)$$

where: $V_{RMS} = \frac{V_{peak}}{\sqrt{2}}$ is the **RMS** or “**effective**” voltage magnitude of the AC waveform.

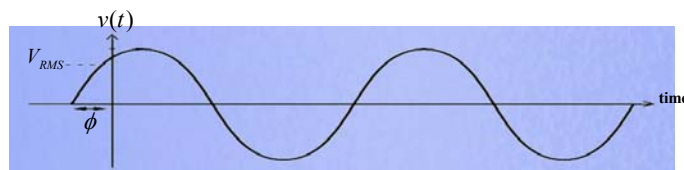
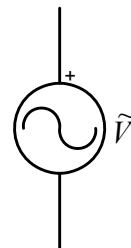


Single-Phase AC Voltage Sources

When performing a steady-state AC analysis, voltages (and currents) are often expressed in “**phasor**” form:

$$\tilde{V} = V e^{j\phi} = V \angle \phi$$

where: V is the RMS magnitude of the voltage, and ϕ is the phase angle of the waveform.

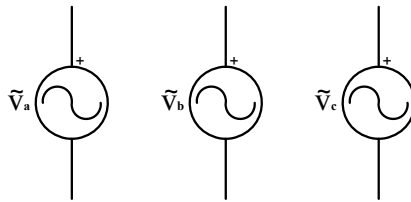




Three-Phase AC Voltage Sources

A *three-phase* (3Φ) *AC voltage* source is a composite source that can be modeled using three single-phase AC voltage sources that are connected together to function as one complete unit.

Note that the three single-phase AC voltage sources must be connected together in a symmetrical fashion.



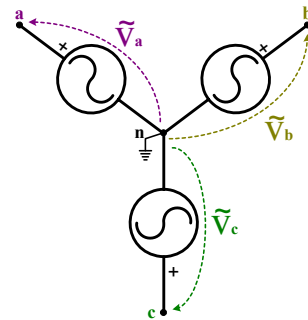
Wye-connected Three-Phase Source

The three sources are typically connected together in a “*Wye*” (*Y*) format such that the reference terminals of the three supplies are tied to a common point of connection.

The common point of connection is referred to as the “*neutral point*”.

(node *n* in the figure)

Note that the neutral point is often grounded in order to provide a zero-volt reference for the source.

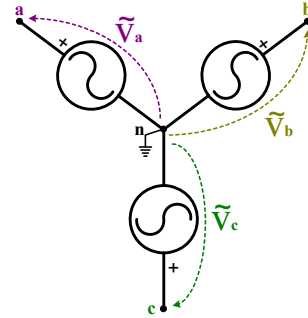




Wye-connected Three-Phase Source

If the remaining nodes are labeled **a**, **b**, and **c**, then:

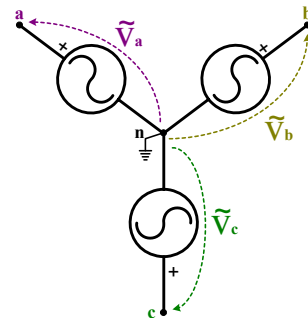
- Then the voltage \tilde{V}_a can be defined as the voltage-rise from the neutral point **n** to node **a**.
- Similarly, voltages \tilde{V}_b and \tilde{V}_c can be defined as the rises from node **n** to **b** and node **n** to **c** respectively.



Phase Voltages

The voltages \tilde{V}_a , \tilde{V}_b , and \tilde{V}_c are referred to as “*phase voltages*” because they correspond to the voltage across each individual phase of the wye-connected source.

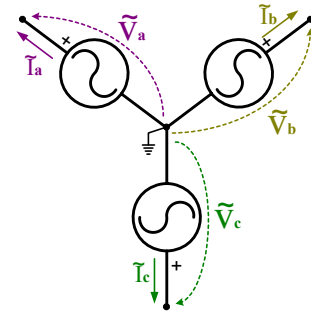
The phase voltages are sometimes referred to as “*line-to-neutral voltages*”, and as such may be expressed as \tilde{V}_{an} , \tilde{V}_{bn} , and \tilde{V}_{cn} .





Phase Currents

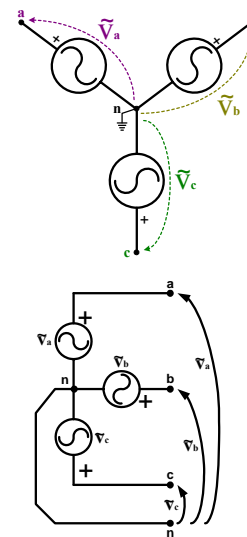
Similarly, the currents \tilde{I}_a , \tilde{I}_b , and \tilde{I}_c are referred to as “*phase currents*” because they correspond to the current flowing through each individual phase of the wye-connected source.



Wye-connected Three-Phase Source

Both of the figures shown to the right depict the same 3 Φ source. The only differences are that the bottom figure has the three phases drawn in either a vertical or a horizontal orientation and a that wire has been connected to the neutral point to provide a fourth point of connection.

Note that the phase voltages are also shown in the bottom figure, but this time with respect to the four point of connection, terminals **a**, **b**, **c**, and **n**.



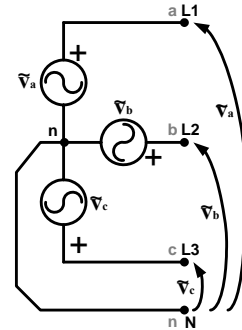


Wye-connected Source Terminals

The primary source terminals or connection points are nodes **a**, **b**, and **c**.

Nodes **a**, **b**, and **c** are sometimes defined as *line terminals L1, L2, and L3* because they are the terminals to which the three lines of a 3 Φ transmission line (cable) will be connected.

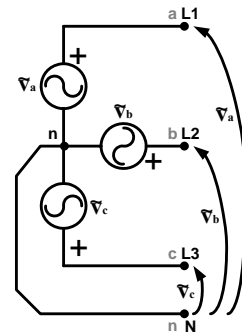
The line connected to the neutral-point is often referred to as the “*neutral line*”.



Balanced Three-Phase Voltage Source

A “*balanced*” 3 Φ source is a source whose phase voltages have equal magnitudes and phase angles that are separated by 120°.

Note that, despite slight magnitude differences that might exist between the three individual phases, most practical 3 Φ sources are assumed to be balanced.





Balanced Phase Voltages

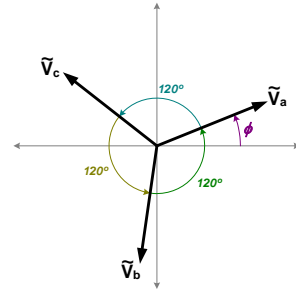
If expressed as phasors, a balanced set of the phase voltages can be defined as follows:

$$\tilde{V}_a = V \angle \phi$$

$$\tilde{V}_b = V \angle \phi - 120^\circ$$

$$\tilde{V}_c = V \angle \phi - 240^\circ$$

where: V is the RMS magnitude of the voltages, and
 ϕ is the phase angle of the phase **a** source.



Phase Voltages

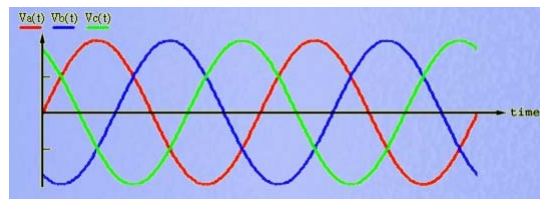
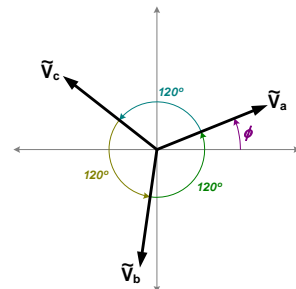
The figure below is a plot of a balanced set of phase voltages:

$$\tilde{V}_a = V \angle \phi$$

$$\tilde{V}_b = V \angle \phi - 120^\circ$$

$$\tilde{V}_c = V \angle \phi - 240^\circ$$

as a function of time with $\phi = 0^\circ$ as shown.





Phase Sequence

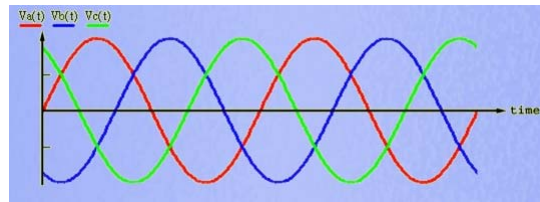
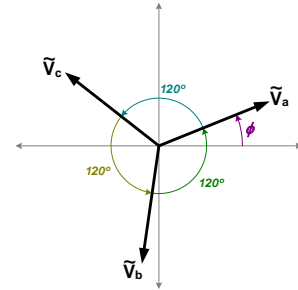
Note that the voltage relationships:

$$\tilde{V}_a = V \angle \phi$$

$$\tilde{V}_b = V \angle \phi - 120^\circ$$

$$\tilde{V}_c = V \angle \phi - 240^\circ$$

define a “*positive-sequence*” (*a-b-c*) source since phase **a** leads **b** and phase **b** leads **c**.



Phase Voltage Example

Given the phase voltage:

$$\tilde{V}_a = 120 \angle 40^\circ$$

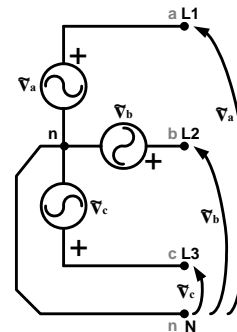
determine the other phase voltages \tilde{V}_b and \tilde{V}_c .

If $\tilde{V}_a = V \angle \phi$, then $V = 120$ volts and $\phi = 40^\circ$, thus:

$$\tilde{V}_a = V \angle \phi = 120 \angle 40^\circ$$

$$\tilde{V}_b = V \angle \phi - 120^\circ = 120 \angle -80^\circ \rightarrow \tilde{V}_b = 120 \angle -80^\circ$$

$$\tilde{V}_c = V \angle \phi - 240^\circ = 120 \angle -200^\circ \rightarrow \tilde{V}_c = 120 \angle -200^\circ$$



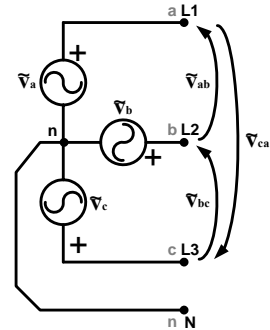


Line Voltages

A second set of voltages can also be defined for the 3Φ source in terms of the voltage rise between each pair of terminals:

a-b, b-c, and c-a.

The voltages \tilde{V}_{ab} , \tilde{V}_{bc} and \tilde{V}_{ca} are referred to as “*line voltages*” because they are the voltages between any pair of line terminals.

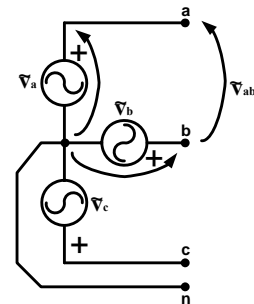


Line Voltages

The *line voltages* for a balanced 3Φ source are closely related to the source's phase voltages.

For example, the line voltage defines the \tilde{V}_{ab} voltage rise from terminal **b** to terminal **a**, and can be expressed in terms of the phase voltages by the KVL equation:

$$\tilde{V}_{ab} = -\tilde{V}_b + \tilde{V}_a = \tilde{V}_a - \tilde{V}_b$$





Line Voltages

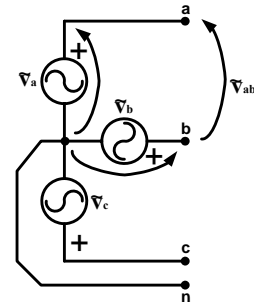
The **line voltages** for a balanced 3 Φ source are closely related to the source's phase voltages.

The same logic can be used to express all three line voltages in terms of their respective phase voltages:

$$\tilde{V}_{ab} = \tilde{V}_a - \tilde{V}_b$$

$$\tilde{V}_{bc} = \tilde{V}_b - \tilde{V}_c$$

$$\tilde{V}_{ca} = \tilde{V}_c - \tilde{V}_a$$



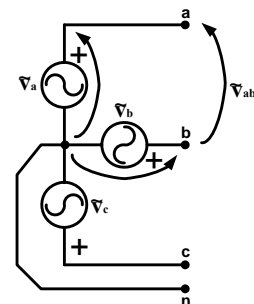
Line Voltages

Given a balanced 3 Φ source that has the phase voltage:

$$\tilde{V}_a = V \angle \phi^\circ$$

the **line voltage** \tilde{V}_{ab} for that source can be determined as follows:

$$\begin{aligned} \tilde{V}_{ab} &= \tilde{V}_a - \tilde{V}_b \\ &= V \angle \phi^\circ - V \angle \phi - 120^\circ \\ &= \sqrt{3} \cdot V \angle \phi + 30^\circ \end{aligned}$$





Line Voltages

A complete analysis of a 3 Φ source having the phase voltages:

$$\tilde{V}_a = V \angle \phi^\circ$$

$$\tilde{V}_b = V \angle \phi - 120^\circ$$

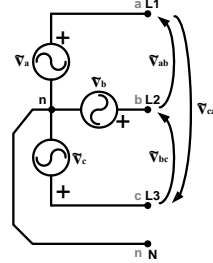
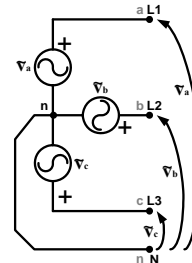
$$\tilde{V}_c = V \angle \phi - 240^\circ$$

will result in the following set of line voltages:

$$\tilde{V}_{ab} = \sqrt{3} \cdot V \angle \phi + 30^\circ$$

$$\tilde{V}_{bc} = \sqrt{3} \cdot V \angle \phi - 90^\circ$$

$$\tilde{V}_{ca} = \sqrt{3} \cdot V \angle \phi - 210^\circ$$



Line Voltages

Note that the line voltages have equal magnitudes and a 120° phase separation between each pair;

Thus, the line voltages maintain the same **balanced** relationship as the phase voltages:

Phase Voltages

$$\tilde{V}_a = V \angle \phi$$

$$\tilde{V}_b = V \angle \phi - 120^\circ$$

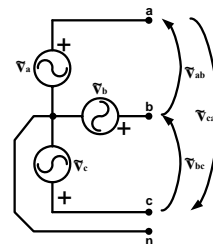
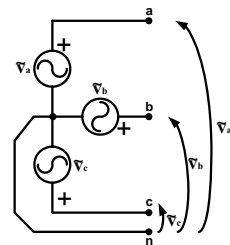
$$\tilde{V}_c = V \angle \phi - 240^\circ$$

Line Voltages

$$\tilde{V}_{ab} = \sqrt{3} \cdot V \angle \phi + 30^\circ$$

$$\tilde{V}_{bc} = \sqrt{3} \cdot V \angle \phi - 90^\circ$$

$$\tilde{V}_{ca} = \sqrt{3} \cdot V \angle \phi - 210^\circ$$





Phase ↔ Line Voltage Relationship

A comparison of the phase and line voltages:

$$\tilde{V}_a = V \angle \phi^\circ \quad \tilde{V}_{ab} = \sqrt{3} \cdot V \angle \phi + 30^\circ$$

reveals that the line voltages are:

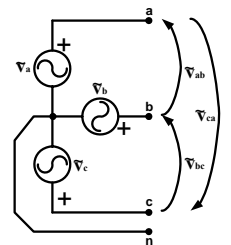
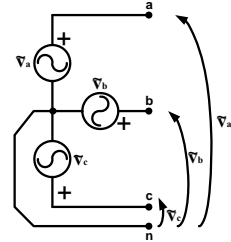
- $\sqrt{3}$ x greater in magnitude, and
- 30° greater in phase angle

compared to the phase voltages.

$$\tilde{V}_{ab} = (\sqrt{3} \angle 30^\circ) \cdot \tilde{V}_a$$

$$\tilde{V}_{bc} = (\sqrt{3} \angle 30^\circ) \cdot \tilde{V}_b$$

$$\tilde{V}_{ca} = (\sqrt{3} \angle 30^\circ) \cdot \tilde{V}_c$$



Phase ↔ Line Voltage Relationship

Thus, given a balanced 3 Φ source, the following phase-to-line voltage relationships can be used to specify the complete set of phase and line voltages:

Phase Voltages

$$\tilde{V}_a = V \angle \phi$$

$$\tilde{V}_b = V \angle \phi - 120^\circ$$

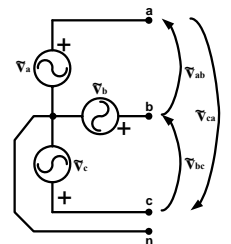
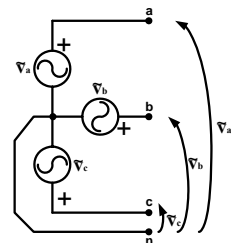
$$\tilde{V}_c = V \angle \phi - 240^\circ$$

Line Voltages

$$\tilde{V}_{ab} = \sqrt{3} \cdot V \angle \phi + 30^\circ$$

$$\tilde{V}_{bc} = \sqrt{3} \cdot V \angle \phi - 90^\circ$$

$$\tilde{V}_{ca} = \sqrt{3} \cdot V \angle \phi - 210^\circ$$





Line Voltage Example

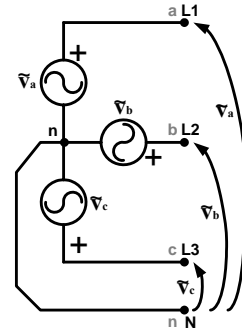
Given a 3 Φ source with phase voltages:

$$\tilde{V}_a = 120 \angle 40^\circ$$

$$\tilde{V}_b = 120 \angle -80^\circ$$

$$\tilde{V}_c = 120 \angle -200^\circ$$

determine the line voltages \tilde{V}_{ab} , \tilde{V}_{bc} and \tilde{V}_{ca} .



$$\tilde{V}_{ab} = (\sqrt{3} \angle 30^\circ) \cdot \tilde{V}_a = (\sqrt{3} \angle 30^\circ) \cdot 120 \angle 40^\circ = 208 \angle 70^\circ$$

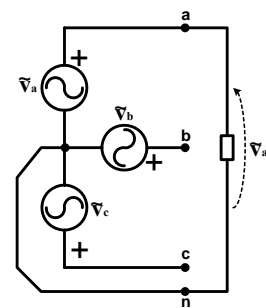
$$\tilde{V}_{bc} = (\sqrt{3} \angle 30^\circ) \cdot \tilde{V}_b = (\sqrt{3} \angle 30^\circ) \cdot 120 \angle -80^\circ = 208 \angle -50^\circ$$

$$\tilde{V}_{ca} = (\sqrt{3} \angle 30^\circ) \cdot \tilde{V}_c = (\sqrt{3} \angle 30^\circ) \cdot 120 \angle -200^\circ = 208 \angle -170^\circ$$

1 Φ Voltages Available from 3 Φ Source

A **single-phase load** may be supplied from a three-phase source if the load is connected across two of the source's terminals.

If the load is connected between a line terminal and the neutral terminal, then a **phase voltage** will appear across the load.

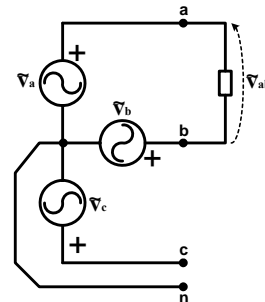




1 Φ Voltages Available from 3 Φ Source

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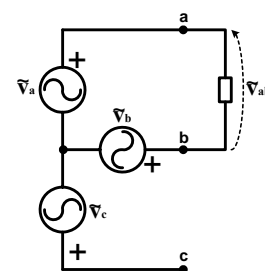
If the load is connected between two of the line terminals, then a **line voltage** will appear across the load.



1 Φ Voltages Available from 3 Φ Source

A **single-phase load** may be supplied from a three-phase source if the load is connected across two of the source's terminals.

If the load is connected between two of the line terminals, then a **line voltage** will appear across the load.



Note – if the neutral terminal is not available, then only the **line voltages** can be received from the supply and not the phase voltages.





Balanced Three-Phase Loads

A *three-phase load* consists of three individual loads that are connected together to form a symmetrical, composite load that is supplied by a 3Φ source.

A *balanced* 3Φ load is constructed using three loads that all have the same impedance value.

When a balanced 3Φ load is connected to a balanced 3Φ source, the resultant currents will also maintain a balanced relationship similar to that of the phase or line voltages.



Three-Phase Load Configurations

There are two different load configurations that can be utilized in order to connect the three individual loads together in a symmetrical manner:

- Wye (Y)
- Delta (Δ)

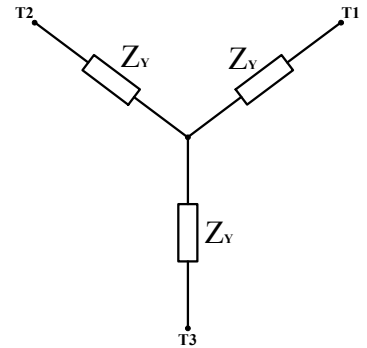


Wye-connected Three-Phase Loads

A *wye-connected*, three-phase load is constructed by connecting one end of the three individual loads to form a common (neutral) node.

The opposite end of the three individual loads provide the terminals for connection to a 3Φ system.

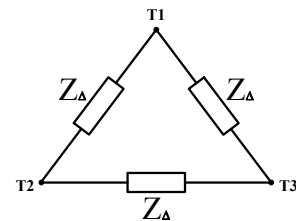
These terminals are often defined as load terminals **T1**, **T2**, and **T3**.



Delta-connected Three-Phase Loads

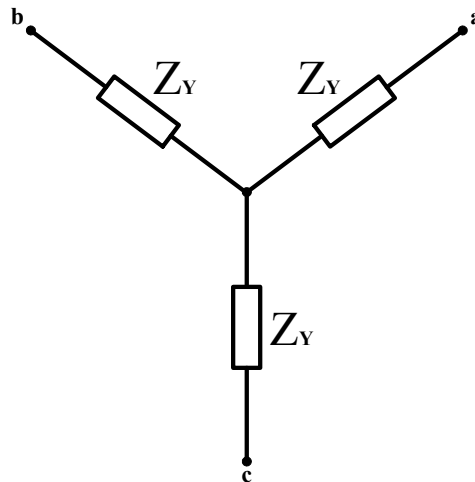
A *delta-connected*, three-phase load is constructed by connecting three impedances together as shown to the right.

The three nodes that connect each pair of impedances provide the terminals for connection to a 3Φ system.





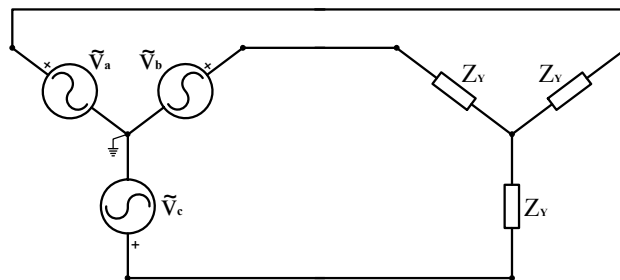
Wye-connected Three-Phase Loads



Wye-connected Loads in 3 Φ Systems

The simple 3 Φ system shown below consists of a *wye-connected source* and a *wye-connected load*.

The neutral-point of the source is grounded to provide a zero-volt reference for the system.

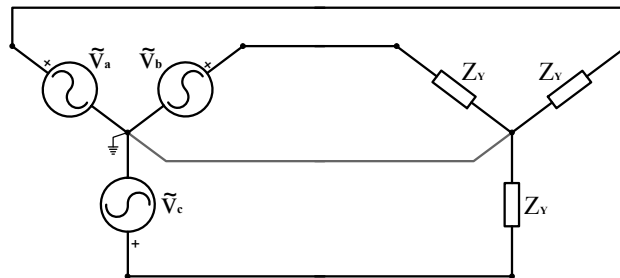




Wye-connected Loads in 3Φ Systems

Three wires or “*lines*” are used to connect the source terminals to the terminals of the Y-connected load.

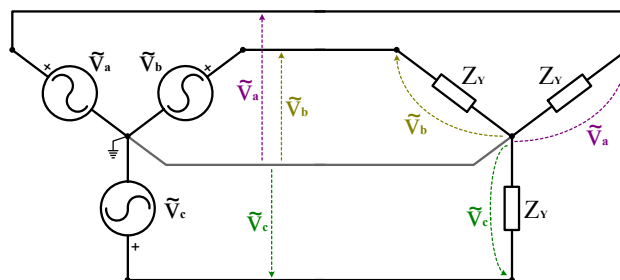
A “*neutral wire*” can be added to connect the grounded neutral-point of the source to the center-point of the load, holding both neutral points at a zero-volt potential.



Wye-connected Loads in 3Φ Systems

Note that the voltage potential present on each line (w.r.t. the neutral wire) is equal to the *phase voltage* of the source’s phase to which the line is connected.

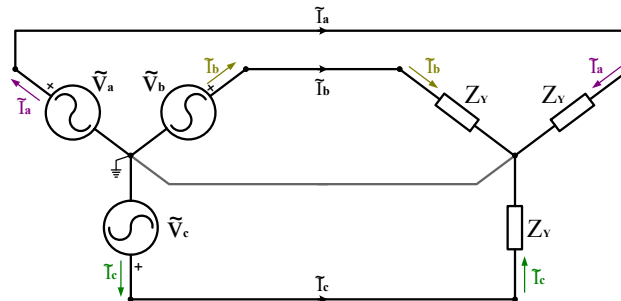
Thus, the four-wire connection results in the presence of a *phase voltage* across each phase of the load.





Wye-connected Load Currents

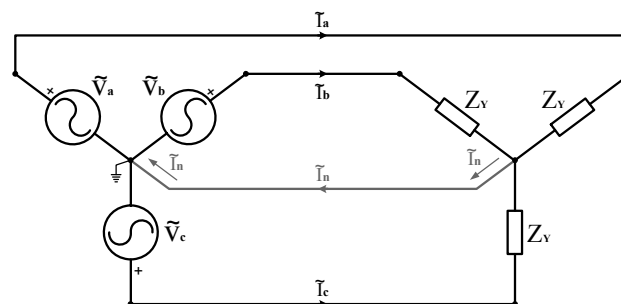
A set of *line currents* (\tilde{I}_a , \tilde{I}_b and \tilde{I}_c) can be defined that flow from each phase of the source, down the lines and into the individual phases of the load.



Wye-connected Load Currents

A set of *line currents* (\tilde{I}_a , \tilde{I}_b and \tilde{I}_c) can be defined that flow from each phase of the source, down the lines and into the individual phases of the load.

A *neutral current* (\tilde{I}_n) can also be defined that flows in the neutral wire from the load back to the source.



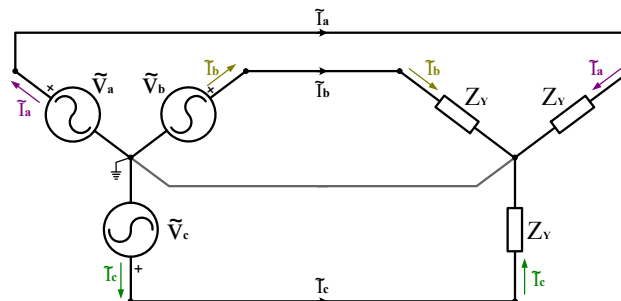


Wye-connected Load Currents

Note that the *line currents* may also be referred to as

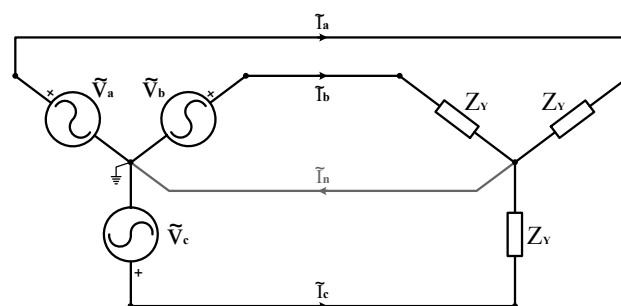
- *phase currents of the source*, or
- *phase currents of the load*

because they flow through the individual phases of both the source and the load.



Wye-connected Load Currents

If the source voltages and load impedances are all known, then the *line currents* and the *neutral current* can all be determined using basic circuit theory.

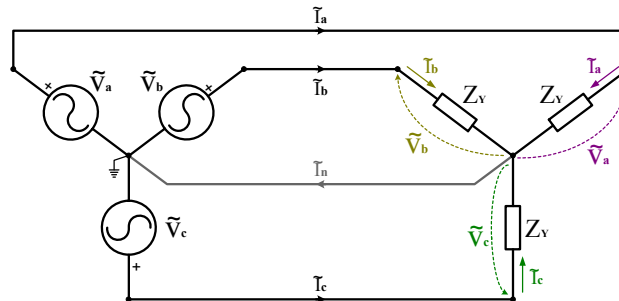




Wye-connected Load Currents

Since the phase voltages of the load and source are equal, the line currents can each be solved independently by applying Ohm's Law at each load.

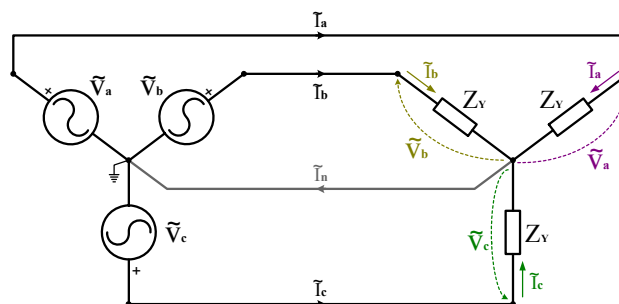
$$\tilde{I}_a = \frac{\tilde{V}_a}{Z_Y} \quad \tilde{I}_b = \frac{\tilde{V}_b}{Z_Y} \quad \tilde{I}_c = \frac{\tilde{V}_c}{Z_Y}$$



Wye-connected Load Currents

Furthermore, if the source voltages are balanced and the load impedances are all equal, then the line currents will also be balanced.

$$\tilde{I}_a = I \angle \delta \quad \tilde{I}_b = I \angle \delta - 120^\circ \quad \tilde{I}_c = I \angle \delta - 240^\circ$$

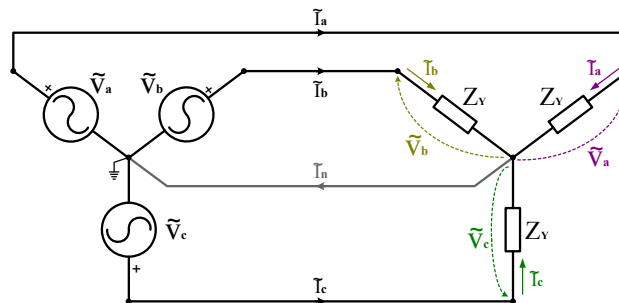




Complex Power in 3Φ Systems

The total complex power produced or consumed by a 3Φ source or load is equal to the sum of the complex powers produced or consumed by each of the source's or load's three individual phases.

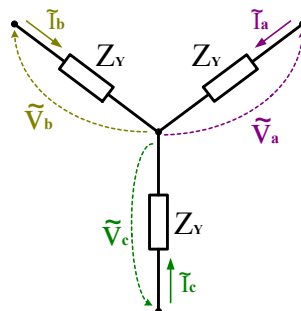
$$S_{3\Phi} = S_a + S_b + S_c$$



Complex Power in Y-connected Loads

In the case of a 3Φ, Y-connected load, the complex powers consumed by each of the load's three individual phases are:

$$S_a = \tilde{V}_a \cdot \tilde{I}_a^* \quad S_b = \tilde{V}_b \cdot \tilde{I}_b^* \quad S_c = \tilde{V}_c \cdot \tilde{I}_c^*$$





Complex Power in Y-connected Loads

If the system is balanced, with voltages and currents:

$$\begin{aligned}\tilde{V}_a &= V\angle\phi & \tilde{I}_a &= I\angle\delta \\ \tilde{V}_b &= V\angle\phi - 120^\circ & \tilde{I}_b &= I\angle\delta - 120^\circ \\ \tilde{V}_c &= V\angle\phi - 240^\circ & \tilde{I}_c &= I\angle\delta - 240^\circ\end{aligned}$$

then:

$$\begin{aligned}S_a &= \tilde{V}_a \cdot \tilde{I}_a^* = [V\angle\phi] \cdot [I\angle -(\delta)] & &= V \cdot I\angle\phi - \delta \\ S_b &= \tilde{V}_b \cdot \tilde{I}_b^* = [V\angle\phi - 120^\circ] \cdot [I\angle -(\delta - 120^\circ)] & &= V \cdot I\angle\phi - \delta \\ S_c &= \tilde{V}_c \cdot \tilde{I}_c^* = [V\angle\phi - 240^\circ] \cdot [I\angle -(\delta - 240^\circ)] & &= V \cdot I\angle\phi - \delta\end{aligned}$$



Complex Power in Y-connected Loads

If the system is balanced, with voltages and currents:

$$\begin{aligned}\tilde{V}_a &= V\angle\phi & \tilde{I}_a &= I\angle\delta \\ \tilde{V}_b &= V\angle\phi - 120^\circ & \tilde{I}_b &= I\angle\delta - 120^\circ \\ \tilde{V}_c &= V\angle\phi - 240^\circ & \tilde{I}_c &= I\angle\delta - 240^\circ\end{aligned}$$

then:

$$\begin{aligned}S_a &= \tilde{V}_a \cdot \tilde{I}_a^* = V \cdot I\angle\phi - \delta \\ S_b &= \tilde{V}_b \cdot \tilde{I}_b^* = V \cdot I\angle\phi - \delta \\ S_c &= \tilde{V}_c \cdot \tilde{I}_c^* = V \cdot I\angle\phi - \delta\end{aligned}$$

all three phases
will consume equal
complex powers.



Complex Power in Y-connected Loads

Thus, the total complex power consumed by a balanced, 3 Φ , Y-connected load will be equal to 3x the power consumed by any individual phase:

$$S_{3\Phi} = S_a + S_b + S_c = 3 \cdot S_{1\Phi}$$

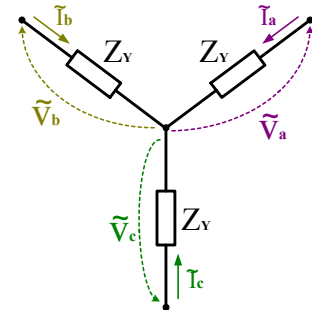
allowing the total complex power to be expressed in terms of a single phase:

$$S_{3\Phi} = 3 \cdot \tilde{V}_a \cdot \tilde{I}_a^* = 3 \cdot V \cdot I \angle \phi - \delta$$

where:

$$\tilde{V}_a = V \angle \phi$$

$$\tilde{I}_a = I \angle \delta$$



Complex Power in Y-connected Sources

Additionally, the total complex power produced by a balanced, 3 Φ , Y-connected source will be equal to 3x the power produced by any individual phase:

$$S_{3\Phi} = S_a + S_b + S_c = 3 \cdot S_{1\Phi}$$

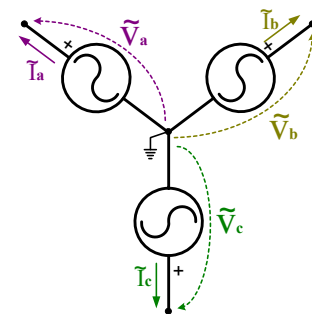
allowing the total complex power to be expressed in terms of a single phase:

$$S_{3\Phi} = 3 \cdot \tilde{V}_a \cdot \tilde{I}_a^* = 3 \cdot V \cdot I \angle \phi - \delta$$

where:

$$\tilde{V}_a = V \angle \phi$$

$$\tilde{I}_a = I \angle \delta$$

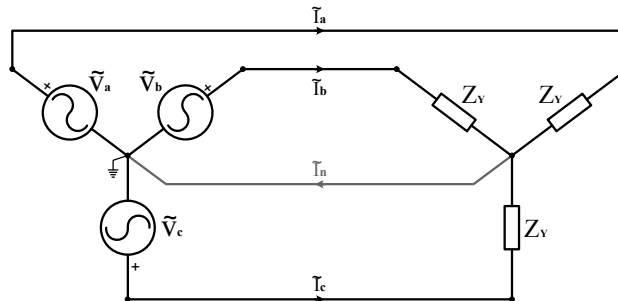




Neutral Current in 3 Φ Systems

The neutral current \tilde{I}_n can be determined by solving the node equation:

$$\tilde{I}_n = \tilde{I}_a + \tilde{I}_b + \tilde{I}_c$$

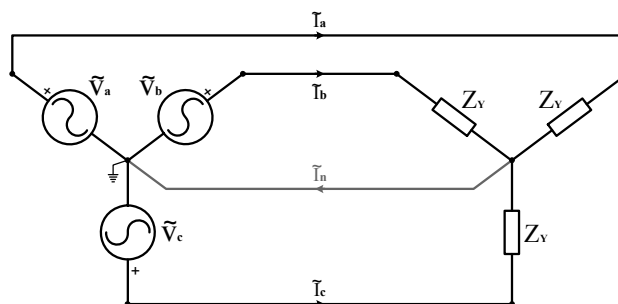


Neutral Current in 3 Φ Systems

In a balanced system, the neutral current will be:

$$\tilde{I}_n = \tilde{I}_a + \tilde{I}_b + \tilde{I}_c = I\angle\delta + I\angle(\delta - 120^\circ) + I\angle(\delta - 240^\circ) = 0$$

If the line currents are balanced, then they will sum to zero
→ no current will flow in the neutral wire.

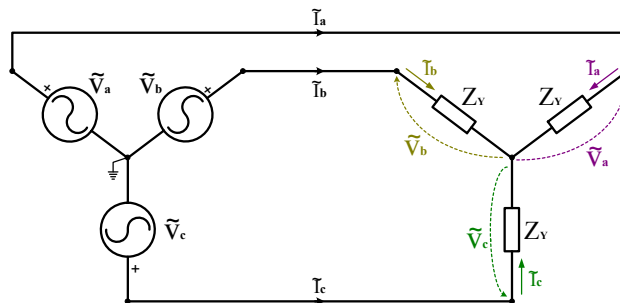




Neutral Wires in 3 Φ Systems

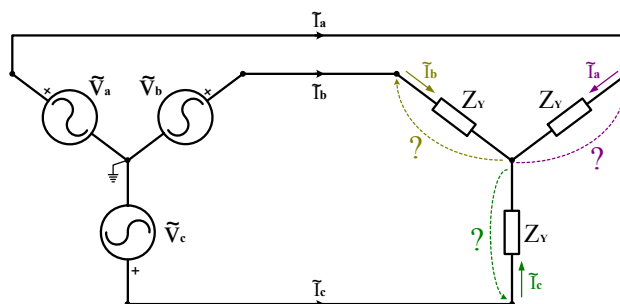
If the system is balanced such that the neutral current is zero,

Then removal of the neutral wire will theoretically have no effect on the operation of the system.



Neutral Wires in 3 Φ Systems

Although removal of the neutral wire will not affect the operation of a balanced system, the importance of the neutral wire comes into play during times of unbalanced operation during which its existence can greatly affect the system.

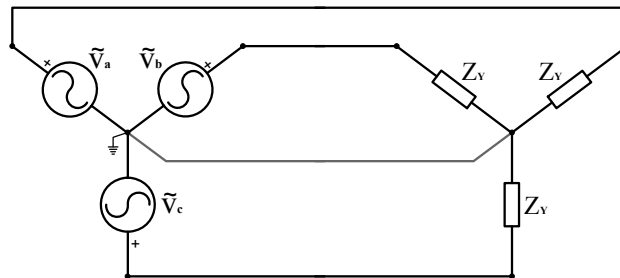




3 Φ Wye-connected Load Example

Given a 480V, 3 Φ , Y-connected, positive-sequence, balanced source that is supplying a Y-connected, balanced load with individual per-phase impedances:

$$Z_Y = 80 + j60 \Omega,$$



3 Φ Wye-connected Load Example

Given a 480V, 3 Φ , Y-connected, positive-sequence, balanced source that is supplying a Y-connected, balanced load with individual per-phase impedances:

$$Z_Y = 80 + j60 \Omega,$$

Determine:

- all of the phase and line voltages in the system,
- all of the line currents in the system, and
- the total complex power provided by the source to the Y- load.

Note – choose the angle of the phase voltage \tilde{V}_a to be the 0° reference angle.



3 Φ Wye-connected Load Example

Since the source is a Y-connected, positive-sequence, balanced source, the phase and line voltages will adhere to the following relationships:

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|---|---|
| $\tilde{V}_a = V \angle \phi$ | $\tilde{V}_{ab} = \sqrt{3} \cdot V \angle \phi + 30^\circ$ |
| $\tilde{V}_b = V \angle \phi - 120^\circ$ | $\tilde{V}_{bc} = \sqrt{3} \cdot V \angle \phi - 90^\circ$ |
| $\tilde{V}_c = V \angle \phi - 240^\circ$ | $\tilde{V}_{ca} = \sqrt{3} \cdot V \angle \phi - 210^\circ$ |

The values of V and ϕ can be determined from the information provided in the problem statement.



3 Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|---|---|
| $\tilde{V}_a = V \angle \phi$ | $\tilde{V}_{ab} = \sqrt{3} \cdot V \angle \phi + 30^\circ$ |
| $\tilde{V}_b = V \angle \phi - 120^\circ$ | $\tilde{V}_{bc} = \sqrt{3} \cdot V \angle \phi - 90^\circ$ |
| $\tilde{V}_c = V \angle \phi - 240^\circ$ | $\tilde{V}_{ca} = \sqrt{3} \cdot V \angle \phi - 210^\circ$ |

Standard: if a single voltage magnitude is specified for a 3 Φ source, then the value specified is the source's line-voltage magnitude.

Thus, given a balanced 480V source, the line and phase voltage magnitudes can all be specified as:

$$V_{line} = \sqrt{3} \cdot V = 480 \text{ volts} \quad \rightarrow \quad V_{phase} = V = \frac{480}{\sqrt{3}} = 277 \text{ volts}$$



3 Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|---|--|
| $\tilde{V}_a = 277\angle\phi$ | $\tilde{V}_{ab} = 480\angle\phi + 30^\circ$ |
| $\tilde{V}_b = 277\angle\phi - 120^\circ$ | $\tilde{V}_{bc} = 480\angle\phi - 90^\circ$ |
| $\tilde{V}_c = 277\angle\phi - 240^\circ$ | $\tilde{V}_{ca} = 480\angle\phi - 210^\circ$ |

Standard: if a single voltage magnitude is specified for a 3 Φ source, then the value specified is the source's line-voltage magnitude.

Note – if the source is Y-connected with an accessible neutral point, then the line and phase voltage magnitudes are often specified for convenience.

I.e. – 480/277V



3 Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|---|--|
| $\tilde{V}_a = 277\angle\phi$ | $\tilde{V}_{ab} = 480\angle\phi + 30^\circ$ |
| $\tilde{V}_b = 277\angle\phi - 120^\circ$ | $\tilde{V}_{bc} = 480\angle\phi - 90^\circ$ |
| $\tilde{V}_c = 277\angle\phi - 240^\circ$ | $\tilde{V}_{ca} = 480\angle\phi - 210^\circ$ |

As with any steady-state AC circuit solution, the first phase angle in a 3 Φ circuit may be chosen arbitrarily, after which all other phase angles (voltage and current) must be calculated based to the initial choice.

For convenience, the first angle is often chosen to be 0 $^\circ$.



3Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|---|--|
| $\tilde{V}_a = 277 \angle \phi$ | $\tilde{V}_{ab} = 480 \angle \phi + 30^\circ$ |
| $\tilde{V}_b = 277 \angle \phi - 120^\circ$ | $\tilde{V}_{bc} = 480 \angle \phi - 90^\circ$ |
| $\tilde{V}_c = 277 \angle \phi - 240^\circ$ | $\tilde{V}_{ca} = 480 \angle \phi - 210^\circ$ |

In this example, the problem statement instructed that an initial angle of 0° was to be chosen for the phase voltage \tilde{V}_a .

Thus, as defined in the relationships shown above:

$$\phi = 0^\circ,$$

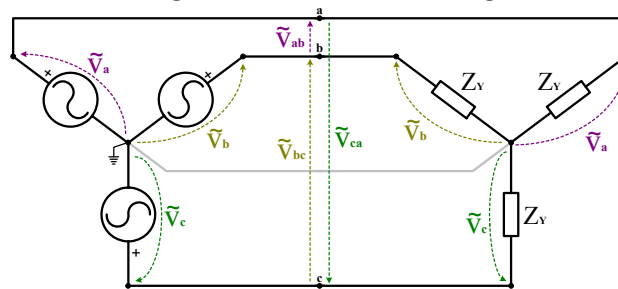
to which all of the other angles can be referenced.



3Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|---------------------------------------|--|
| $\tilde{V}_a = 277 \angle 0^\circ$ | $\tilde{V}_{ab} = 480 \angle +30^\circ$ |
| $\tilde{V}_b = 277 \angle -120^\circ$ | $\tilde{V}_{bc} = 480 \angle -90^\circ$ |
| $\tilde{V}_c = 277 \angle -240^\circ$ | $\tilde{V}_{ca} = 480 \angle -210^\circ$ |

The phase and line voltages are shown in the figure below:





3 Φ Wye-connected Load Example

Phase Voltages

$$\tilde{V}_a = 277 \angle 0^\circ$$

$$\tilde{V}_b = 277 \angle -120^\circ$$

$$\tilde{V}_c = 277 \angle -240^\circ$$

Line Voltages

$$\tilde{V}_{ab} = 480 \angle +30^\circ$$

$$\tilde{V}_{bc} = 480 \angle -90^\circ$$

$$\tilde{V}_{ca} = 480 \angle -210^\circ$$

Now that all of the voltages have been specified in the system, the next step is to solve for all of the line currents that will flow in the 3 Φ system from the source to the load.



3 Φ Wye-connected Load Example

Phase Voltages

$$\tilde{V}_a = 277 \angle 0^\circ$$

$$\tilde{V}_b = 277 \angle -120^\circ$$

$$\tilde{V}_c = 277 \angle -240^\circ$$

Line Voltages

$$\tilde{V}_{ab} = 480 \angle +30^\circ$$

$$\tilde{V}_{bc} = 480 \angle -90^\circ$$

$$\tilde{V}_{ca} = 480 \angle -210^\circ$$

Since both the source and the load are both balanced, the resultant line currents will also be balanced.

Because of this, the complete set of line currents may be determined by first solving for one of the currents and then utilizing the balanced relationship in order to specify the remaining currents.



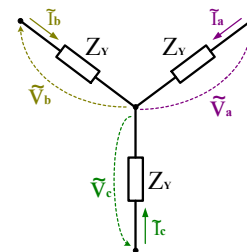
3Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|--------------------------------------|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ |

Applying Ohm's Law to "*phase a*" of the load results the line current:

$$\tilde{I}_a = \frac{\tilde{V}_a}{Z_Y} = \frac{277\angle 0^\circ}{80 + j60} = 2.77\angle -36.9^\circ$$

from which the remaining line currents can be solved.



3Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> |
|--------------------------------------|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ |

Given: $\tilde{I}_a = 2.77\angle -36.9^\circ \rightarrow I = 2.77 \quad \delta = -36.9^\circ$

The remaining line currents can be determined from:

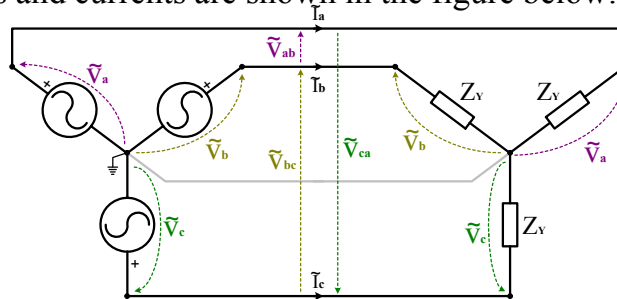
| <u>Balanced Relationships</u> | <u>Line Currents</u> |
|--|---|
| $\tilde{I}_a = I\angle \delta$ | $\tilde{I}_a = 2.77\angle -36.9^\circ$ |
| $\tilde{I}_b = I\angle \delta - 120^\circ$ | $\tilde{I}_b = 2.77\angle -156.9^\circ$ |
| $\tilde{I}_c = I\angle \delta - 240^\circ$ | $\tilde{I}_c = 2.77\angle -276.9^\circ$ |



3Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_a = 2.77\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_b = 2.77\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_c = 2.77\angle -276.9^\circ$ |

The voltages and currents are shown in the figure below:



3Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_a = 2.77\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_b = 2.77\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_c = 2.77\angle -276.9^\circ$ |

Now that all of the voltages and currents have been specified in the system, the next step is to solve for the total complex power that will be provided from the 3Φ source to the 3Φ load.



3 Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_a = 2.77\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_b = 2.77\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_c = 2.77\angle -276.9^\circ$ |

Since the total complex power produced/consumed in a balanced, 3 Φ system is equal to 3x the complex power produced/consumed in a any individual phase:

$$\begin{aligned} S_{3\Phi} &= 3 \cdot \tilde{V}_a \cdot \tilde{I}_a^* = 3 \cdot [277\angle 0^\circ] \cdot [2.77\angle -(-36.9^\circ)] \\ &= 3 \cdot [614.4 + j460.8] = 1843.2 + j1382.4 \end{aligned}$$



3 Φ Wye-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_a = 2.77\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_b = 2.77\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_c = 2.77\angle -276.9^\circ$ |

If desired, the complex power result:

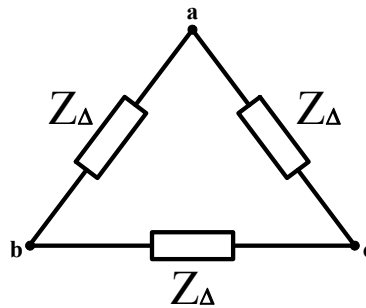
$$S_{3\Phi} = 1843.2 + j1382.4$$

can be broken down into its real and reactive power components:

$$P_{3\Phi} = 1843.2 \text{ Watts} \quad Q_{3\Phi} = 1382.4 \text{ Vars}$$



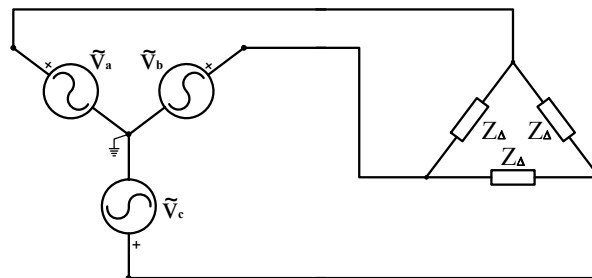
Delta-connected Three-Phase Loads



Delta-connected Loads in 3Φ Systems

The simple 3Φ system shown below consists of a *wye-connected source* and a *delta-connected load*.

The neutral-point of the source is still grounded to provide a zero-volt reference for the system.

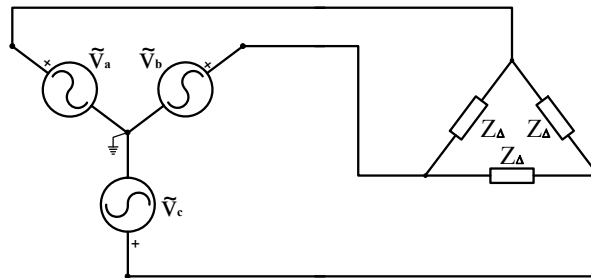




Delta-connected Loads in 3 Φ Systems

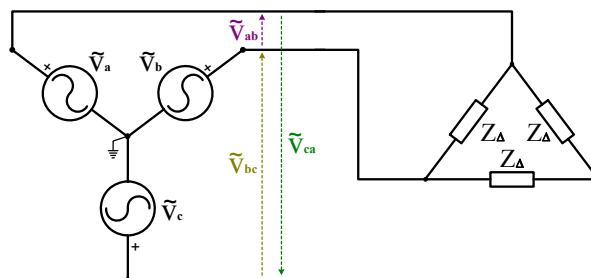
Three “*lines*” are also used to connect the source terminals to the terminals of the Δ -connected load.

Note that no neutral wire can be connected to the load because the Δ -connected load has no central node to which the wire can be symmetrically connected.



Delta-connected Load Voltages

The voltage potential between each pair of lines is equal to the *line voltage* of the source.

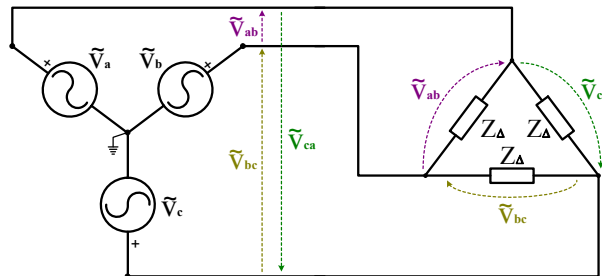




Delta-connected Load Voltages

The voltage potential between each pair of lines is equal to the line voltage of the source.

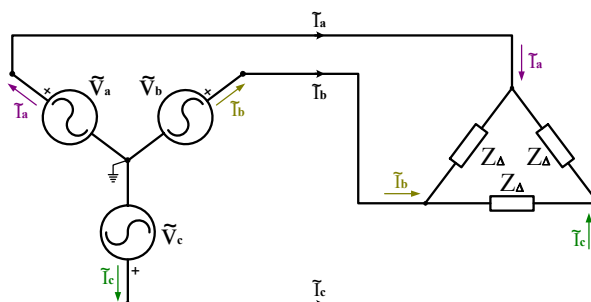
Since each phase of the Δ -connected load connects across a pair of lines, the three-wire connection provides a ***line voltage*** across each phase of the load.



Delta-connected Load Currents

A set of ***line currents*** (\tilde{I}_a , \tilde{I}_b and \tilde{I}_c) was defined to flow in the lines from the source to the load.

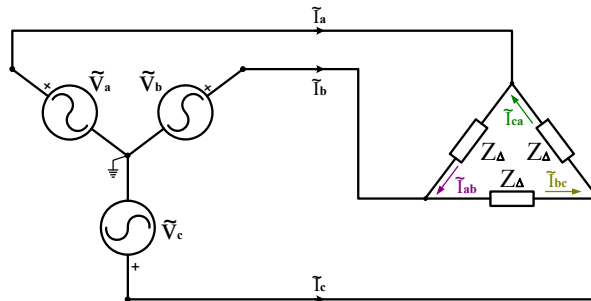
Although the line currents flow through each phase of the source, they do **not** flow through the individual phases of the Δ -load.





Delta-connected Load Currents

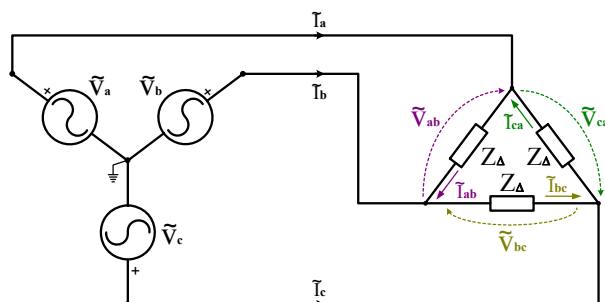
In order to fully characterize the Δ -connected load's operation, a set of ***phase currents*** (\tilde{I}_{ab} , \tilde{I}_{bc} and \tilde{I}_{ca}) that flow through the individual phases of the load must also be defined.



Delta-connected Load Currents

If the line voltages and load impedances are known, then the ***phase currents of the load*** can each be solved independently by applying Ohm's Law for each phase:

$$\tilde{I}_{ab} = \frac{\tilde{V}_{ab}}{Z_{\Delta}} \quad \tilde{I}_{bc} = \frac{\tilde{V}_{bc}}{Z_{\Delta}} \quad \tilde{I}_{ca} = \frac{\tilde{V}_{ca}}{Z_{\Delta}}$$

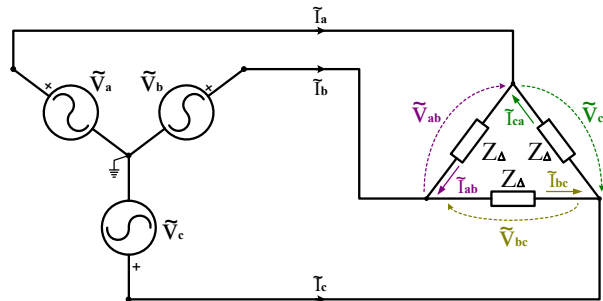




Delta-connected Load Currents

Furthermore, if the source voltages are balanced and the load impedances are all equal, then the phase currents of the load will also be balanced.

$$\tilde{I}_{ab} = I_{\Delta} \angle \beta \quad \tilde{I}_{bc} = I_{\Delta} \angle \beta - 120^{\circ} \quad \tilde{I}_{ca} = I_{\Delta} \angle \beta - 240^{\circ}$$



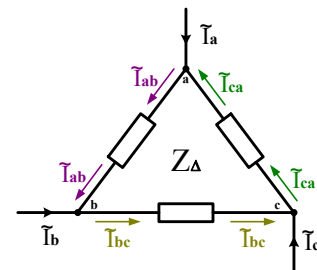
Delta-connected Load Currents

Once the phase currents of the load have been determined, the *line currents* flowing into the load may also be determined by solving a node equation for each of the three connection points to the load.

Node a: $\tilde{I}_a = \tilde{I}_{ab} - \tilde{I}_{ca}$

Node b: $\tilde{I}_b = \tilde{I}_{bc} - \tilde{I}_{ab}$

Node c: $\tilde{I}_c = \tilde{I}_{ca} - \tilde{I}_{bc}$





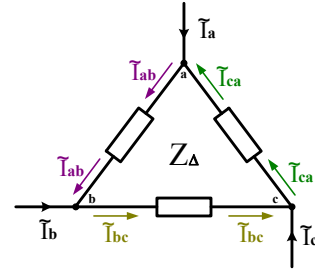
Delta-connected Load Currents

Given the balanced set of phase currents:

$$\tilde{I}_{ab} = I_{\Delta} \angle \beta \quad \tilde{I}_{bc} = I_{\Delta} \angle \beta - 120^{\circ} \quad \tilde{I}_{ca} = I_{\Delta} \angle \beta - 240^{\circ}$$

the line current \tilde{I}_a can be determined as follows:

$$\begin{aligned} \tilde{I}_a &= \tilde{I}_{ab} - \tilde{I}_{ca} \\ &= I_{\Delta} \angle \beta - I_{\Delta} \angle (\beta - 240^{\circ}) \\ &= \sqrt{3} \cdot I_{\Delta} \angle (\beta - 30^{\circ}) \\ &= (\sqrt{3} \angle -30^{\circ}) \cdot \tilde{I}_{ab} \end{aligned}$$



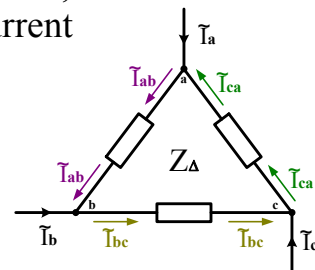
Delta-connected Load Currents

Since the phase currents are balanced:

$$\tilde{I}_{ab} = I_{\Delta} \angle \beta \quad \tilde{I}_{bc} = I_{\Delta} \angle \beta - 120^{\circ} \quad \tilde{I}_{ca} = I_{\Delta} \angle \beta - 240^{\circ}$$

the resultant line currents will also be balanced, allowing a complete set of phase-to-line current relationships to be defined:

$$\begin{aligned} \tilde{I}_a &= (\sqrt{3} \angle -30^{\circ}) \cdot \tilde{I}_{ab} \\ \tilde{I}_b &= (\sqrt{3} \angle -30^{\circ}) \cdot \tilde{I}_{bc} \\ \tilde{I}_c &= (\sqrt{3} \angle -30^{\circ}) \cdot \tilde{I}_{ca} \end{aligned}$$





Phase ↔ Line Current Relationship

The phase-to-line current relationships can then be used to specify a complete set of currents for a balanced, Δ -connected load as follows:

Phase Currents

$$\tilde{I}_{ab} = I_{\Delta} \angle \beta$$

$$\tilde{I}_{bc} = I_{\Delta} \angle \beta - 120^{\circ}$$

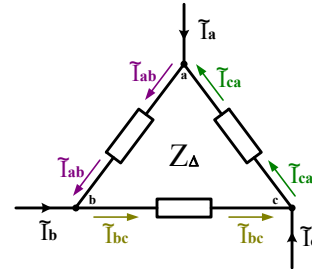
$$\tilde{I}_{ca} = I_{\Delta} \angle \beta - 240^{\circ}$$

Line Currents

$$\tilde{I}_a = \sqrt{3} \cdot I_{\Delta} \angle \beta - 30^{\circ}$$

$$\tilde{I}_b = \sqrt{3} \cdot I_{\Delta} \angle \beta - 150^{\circ}$$

$$\tilde{I}_c = \sqrt{3} \cdot I_{\Delta} \angle \beta - 270^{\circ}$$



Phase ↔ Line Current Relationship

Note – to correspond with the line-currents defined for the Y-connected load, the phase and line current expressions can be rewritten such that:

$$I = \sqrt{3} \cdot I_{\Delta} \quad \delta = \beta - 30^{\circ}$$

Line Currents

$$\tilde{I}_a = I \angle \delta$$

$$\tilde{I}_b = I \angle \delta - 120^{\circ}$$

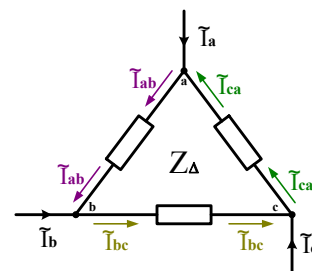
$$\tilde{I}_c = I \angle \delta - 240^{\circ}$$

Phase Currents

$$\tilde{I}_{ab} = \frac{I}{\sqrt{3}} \angle \delta + 30^{\circ}$$

$$\tilde{I}_{bc} = \frac{I}{\sqrt{3}} \angle \delta - 90^{\circ}$$

$$\tilde{I}_{ca} = \frac{I}{\sqrt{3}} \angle \delta - 210^{\circ}$$

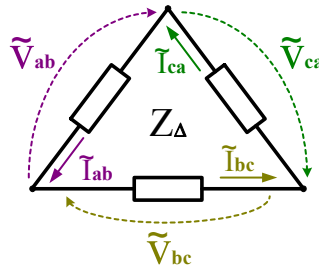




Complex Power in Δ -connected Loads

In the case of a 3 Φ , Δ -connected load, the complex power consumed by each of the load's three individual phases are:

$$S_{ab} = \tilde{V}_{ab} \cdot \tilde{I}_{ab}^* \quad S_{bc} = \tilde{V}_{bc} \cdot \tilde{I}_{bc}^* \quad S_{ca} = \tilde{V}_{ca} \cdot \tilde{I}_{ca}^*$$



Complex Power in Δ -connected Loads

If the system is balanced, with voltages and currents defined as:

$$\begin{aligned} \tilde{V}_{ab} &= \sqrt{3} \cdot V \angle \phi + 30^\circ & \tilde{I}_{ab} &= \frac{I}{\sqrt{3}} \angle \delta + 30^\circ \\ \tilde{V}_{bc} &= \sqrt{3} \cdot V \angle \phi - 90^\circ & \tilde{I}_{bc} &= \frac{I}{\sqrt{3}} \angle \delta - 90^\circ \\ \tilde{V}_{ca} &= \sqrt{3} \cdot V \angle \phi - 210^\circ & \tilde{I}_{ca} &= \frac{I}{\sqrt{3}} \angle \delta - 210^\circ \end{aligned}$$

then:

$$\begin{aligned} S_{ab} &= \tilde{V}_{ab} \cdot \tilde{I}_{ab}^* = \left[\sqrt{3} \cdot V \angle \phi + 30^\circ \right] \cdot \left[\frac{I}{\sqrt{3}} \angle -(\delta + 30^\circ) \right] = V \cdot I \angle \phi - \delta \\ S_{bc} &= \tilde{V}_{bc} \cdot \tilde{I}_{bc}^* = \left[\sqrt{3} \cdot V \angle \phi - 90^\circ \right] \cdot \left[\frac{I}{\sqrt{3}} \angle -(\delta - 90^\circ) \right] = V \cdot I \angle \phi - \delta \\ S_{ca} &= \tilde{V}_{ca} \cdot \tilde{I}_{ca}^* = \left[\sqrt{3} \cdot V \angle \phi - 210^\circ \right] \cdot \left[\frac{I}{\sqrt{3}} \angle -(\delta - 210^\circ) \right] = V \cdot I \angle \phi - \delta \end{aligned}$$



Complex Power in Δ -connected Loads

If the system is balanced, with voltages and currents defined as:

$$\begin{aligned}\tilde{V}_{ab} &= \sqrt{3} \cdot V \angle \phi + 30^\circ & \tilde{I}_{ab} &= \frac{I}{\sqrt{3}} \angle \delta + 30^\circ \\ \tilde{V}_{bc} &= \sqrt{3} \cdot V \angle \phi - 90^\circ & \tilde{I}_{bc} &= \frac{I}{\sqrt{3}} \angle \delta - 90^\circ \\ \tilde{V}_{ca} &= \sqrt{3} \cdot V \angle \phi - 210^\circ & \tilde{I}_{ca} &= \frac{I}{\sqrt{3}} \angle \delta - 210^\circ\end{aligned}$$

then:

$$\begin{aligned}S_{ab} &= \tilde{V}_{ab} \cdot \tilde{I}_{ab}^* = V \cdot I \angle \phi - \delta \\ S_{bc} &= \tilde{V}_{bc} \cdot \tilde{I}_{bc}^* = V \cdot I \angle \phi - \delta \\ S_{ca} &= \tilde{V}_{ca} \cdot \tilde{I}_{ca}^* = V \cdot I \angle \phi - \delta\end{aligned}$$

all three phases will
consume equal
complex power.



Complex Power in Δ -connected Loads

Thus, the total complex power consumed by a balanced, 3Φ , Δ -connected load will be equal to 3x the power consumed by any individual phase:

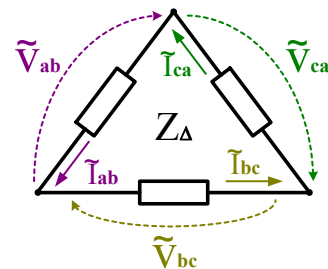
$$S_{3\Phi} = S_{ab} + S_{bc} + S_{ca} = 3 \cdot S_{1\Phi}$$

allowing the total complex power to be expressed in terms of a single phase:

$$S_{3\Phi} = 3 \cdot \tilde{V}_{ab} \cdot \tilde{I}_{ab}^* = 3 \cdot V \cdot I \angle \phi - \delta$$

where:

$$\begin{aligned}\tilde{V}_{ab} &= \sqrt{3} \cdot V \angle \phi + 30^\circ \\ \tilde{I}_{ab} &= \frac{I}{\sqrt{3}} \angle \delta + 30^\circ\end{aligned}$$

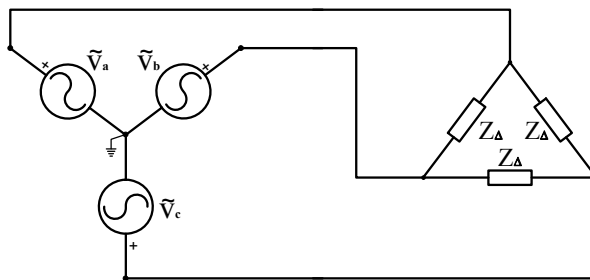




3Φ Delta-connected Load Example

Given a 480V, 3Φ, Y-connected, positive-sequence, balanced source that is supplying a Δ-connected, balanced load with individual phase impedances

$$Z_{\Delta} = 80 + j60 \Omega,$$



3Φ Delta-connected Load Example

Given a 480V, 3Φ, Y-connected, positive-sequence, balanced source that is supplying a Δ-connected, balanced load with individual phase impedances

$$Z_{\Delta} = 80 + j60 \Omega,$$

Determine:

- all of the phase and line voltages in the system,
- all of the phase and line currents in the system, and
- the total complex power provided by the source to the Δ-connected load.

Note – choose the angle of the phase voltage \tilde{V}_a to be the 0° reference angle for the system.



3Φ Delta-connected Load Example

Phase Voltages

$$\tilde{V}_a = 277\angle 0^\circ$$

$$\tilde{V}_b = 277\angle -120^\circ$$

$$\tilde{V}_c = 277\angle -240^\circ$$

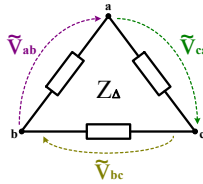
Line Voltages

$$\tilde{V}_{ab} = 480\angle +30^\circ$$

$$\tilde{V}_{bc} = 480\angle -90^\circ$$

$$\tilde{V}_{ca} = 480\angle -210^\circ$$

Since the source defined in this example is the same as that in the Y-connected load example, the phase and line voltages shown above are provided without the logic required to obtain those values.



3Φ Delta-connected Load Example

Phase Voltages

$$\tilde{V}_a = 277\angle 0^\circ$$

$$\tilde{V}_b = 277\angle -120^\circ$$

$$\tilde{V}_c = 277\angle -240^\circ$$

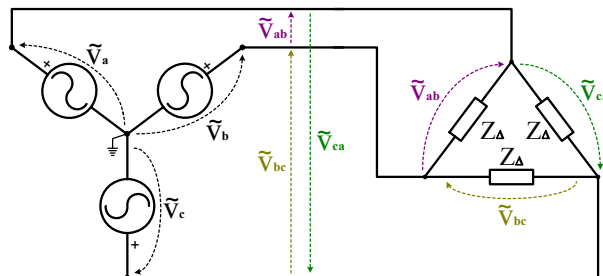
Line Voltages

$$\tilde{V}_{ab} = 480\angle +30^\circ$$

$$\tilde{V}_{bc} = 480\angle -90^\circ$$

$$\tilde{V}_{ca} = 480\angle -210^\circ$$

The phase and line voltages are shown in the figure below:





3Φ Delta-connected Load Example

Line Voltages

$$\tilde{V}_{ab} = 480\angle +30^\circ$$

$$\tilde{V}_{bc} = 480\angle -90^\circ$$

$$\tilde{V}_{ca} = 480\angle -210^\circ$$

Note that although the phase and line voltages both exist at the Y-connected source, only the line voltages appear at the Δ-connected load due to the absence of a neutral point.



3Φ Delta-connected Load Example

Line Voltages

$$\tilde{V}_{ab} = 480\angle +30^\circ$$

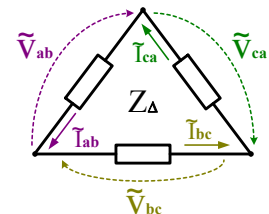
$$\tilde{V}_{bc} = 480\angle -90^\circ$$

$$\tilde{V}_{ca} = 480\angle -210^\circ$$

By applying Ohm's Law to the load connected across nodes **a** and **b**, the phase current can be determined:

$$\tilde{I}_{ab} = \frac{\tilde{V}_{ab}}{Z_\Delta} = \frac{480\angle 30^\circ}{80 + j60} = 4.8\angle -6.9^\circ$$

from which the remaining phase currents can then be solved.





3Φ Delta-connected Load Example

Line Voltages

$$\tilde{V}_{ab} = 480 \angle +30^\circ$$

$$\tilde{V}_{bc} = 480 \angle -90^\circ$$

$$\tilde{V}_{ca} = 480 \angle -210^\circ$$

Given: $\tilde{I}_{ab} = 4.8 \angle -6.9^\circ \rightarrow \frac{I}{\sqrt{3}} = 4.8 \quad \delta + 30^\circ = -6.9^\circ$

The remaining phase currents can be determined from:

Balanced Relationships

$$\tilde{I}_{ab} = \frac{I}{\sqrt{3}} \angle \delta + 30^\circ$$

$$\tilde{I}_{bc} = \frac{I}{\sqrt{3}} \angle \delta - 90^\circ$$

$$\tilde{I}_{ca} = \frac{I}{\sqrt{3}} \angle \delta - 210^\circ$$

Phase Currents

$$\tilde{I}_{ab} = 4.8 \angle -6.9^\circ$$

$$\tilde{I}_{bc} = 4.8 \angle -126.9^\circ$$

$$\tilde{I}_{ca} = 4.8 \angle -246.9^\circ$$

→

3Φ Delta-connected Load Example

Line Voltages

$$\tilde{V}_{ab} = 480 \angle +30^\circ$$

$$\tilde{V}_{bc} = 480 \angle -90^\circ$$

$$\tilde{V}_{ca} = 480 \angle -210^\circ$$

Phase Currents

$$\tilde{I}_{ab} = 4.8 \angle -6.9^\circ$$

$$\tilde{I}_{bc} = 4.8 \angle -126.9^\circ$$

$$\tilde{I}_{ca} = 4.8 \angle -246.9^\circ$$

Additionally: $\frac{I}{\sqrt{3}} = 4.8 \quad \delta + 30^\circ = -6.9^\circ \rightarrow I = 8.31 \quad \delta = -36.9^\circ$

The line currents can be determined from:

Balanced Relationships

$$\tilde{I}_a = I \angle \delta$$

$$\tilde{I}_b = I \angle \delta - 120^\circ$$

$$\tilde{I}_c = I \angle \delta - 240^\circ$$

Line Currents

$$\tilde{I}_a = 8.31 \angle -36.9^\circ$$

$$\tilde{I}_b = 8.31 \angle -156.9^\circ$$

$$\tilde{I}_c = 8.31 \angle -276.9^\circ$$

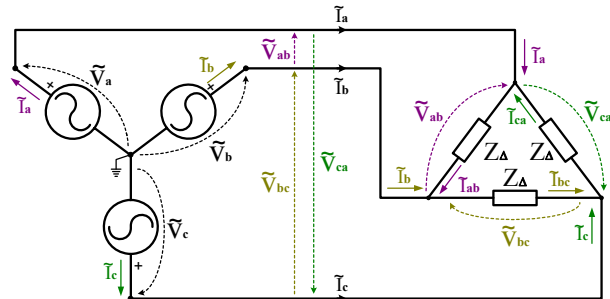
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3Φ Delta-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Phase Currents</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_{ab} = 4.8\angle -6.9^\circ$ | $\tilde{I}_a = 8.31\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_{bc} = 4.8\angle -126.9^\circ$ | $\tilde{I}_b = 8.31\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_{ca} = 4.8\angle -246.9^\circ$ | $\tilde{I}_c = 8.31\angle -276.9^\circ$ |

The voltages and currents are shown in the figure below:



3Φ Delta-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Phase Currents</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_{ab} = 4.8\angle -6.9^\circ$ | $\tilde{I}_a = 8.31\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_{bc} = 4.8\angle -126.9^\circ$ | $\tilde{I}_b = 8.31\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_{ca} = 4.8\angle -246.9^\circ$ | $\tilde{I}_c = 8.31\angle -276.9^\circ$ |

Now that all of the voltages and currents have been specified in the system, the next step is to solve for the total complex power that will be provided by the 3Φ source to the 3Φ load.



3 Φ Delta-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Phase Currents</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_{ab} = 4.8\angle -6.9^\circ$ | $\tilde{I}_a = 8.31\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_{bc} = 4.8\angle -126.9^\circ$ | $\tilde{I}_b = 8.31\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_{ca} = 4.8\angle -246.9^\circ$ | $\tilde{I}_c = 8.31\angle -276.9^\circ$ |

Since the total complex power consumed by a balanced Δ -connected load is equal to 3x the complex power consumed by each individual phase of the load:

$$\begin{aligned} S_{3\Phi} &= 3 \cdot \tilde{V}_{ab} \cdot \tilde{I}_{ab}^* = 3 \cdot [480\angle 30^\circ] \cdot [4.8\angle -(-6.9^\circ)] \\ &= 3 \cdot [1843.2 + j1382.4] = 5529.6 + j4147.2 \end{aligned}$$



3 Φ Delta-connected Load Example

| <u>Phase Voltages</u> | <u>Line Voltages</u> | <u>Phase Currents</u> | <u>Line Currents</u> |
|--------------------------------------|---|---|---|
| $\tilde{V}_a = 277\angle 0^\circ$ | $\tilde{V}_{ab} = 480\angle +30^\circ$ | $\tilde{I}_{ab} = 4.8\angle -6.9^\circ$ | $\tilde{I}_a = 8.31\angle -36.9^\circ$ |
| $\tilde{V}_b = 277\angle -120^\circ$ | $\tilde{V}_{bc} = 480\angle -90^\circ$ | $\tilde{I}_{bc} = 4.8\angle -126.9^\circ$ | $\tilde{I}_b = 8.31\angle -156.9^\circ$ |
| $\tilde{V}_c = 277\angle -240^\circ$ | $\tilde{V}_{ca} = 480\angle -210^\circ$ | $\tilde{I}_{ca} = 4.8\angle -246.9^\circ$ | $\tilde{I}_c = 8.31\angle -276.9^\circ$ |

If desired, the complex power result:

$$S_{3\Phi} = 5529.6 + j4147.2$$

can be broken down into its real and reactive power components:

$$P_{3\Phi} = 5529.6 \text{ Watts} \quad Q_{3\Phi} = 4147.2 \text{ Vars}$$



Y ↔ Δ Load Comparison

Phase Voltages

$$\tilde{V}_a = 277\angle 0^\circ$$

$$\tilde{V}_b = 277\angle -120^\circ$$

$$\tilde{V}_c = 277\angle -240^\circ$$

Line Voltages

$$\tilde{V}_{ab} = 480\angle +30^\circ$$

$$\tilde{V}_{bc} = 480\angle -90^\circ$$

$$\tilde{V}_{ca} = 480\angle -210^\circ$$

Based on the results of the previous examples:

If a balanced 3Φ source is supplying both a Y-connected load and a Δ-connected load, each having the same per-phase impedances:

$$Z_\Delta = Z_Y$$

then the Δ-connected load will consume **3x** more power than the Y-connected load.



Y ↔ Δ Load Comparison

Phase Voltages

$$\tilde{V}_a = 277\angle 0^\circ$$

$$\tilde{V}_b = 277\angle -120^\circ$$

$$\tilde{V}_c = 277\angle -240^\circ$$

Line Voltages

$$\tilde{V}_{ab} = 480\angle +30^\circ$$

$$\tilde{V}_{bc} = 480\angle -90^\circ$$

$$\tilde{V}_{ca} = 480\angle -210^\circ$$

It can also be proven that:

If a balanced 3Φ source is supplying both a Y-connected load and a Δ-connected load, but the per-phase Δ-impedances are **3x** larger than the per-phase Y-impedances:

$$Z_\Delta = 3 \cdot Z_Y$$

then the Δ-connected load and the Y-connected load will consume the **same** amount of power.